and thus that

$$\varepsilon_{cr} \to \frac{(1-a)^3}{4n^2\pi^2}$$
 as  $n \to \infty$  (16)

The estimates of the natural frequencies obtained by the singular perturbation approach will then be accurate when  $\varepsilon < \varepsilon_{cr}$ , or equivalently when  $\varepsilon n^2 < [(1-a)^3/4\pi^2]$  as  $n \to \infty$ .

The closeness of the threshold values  $\varepsilon^*$  [Eq. (13)] and  $\varepsilon_{cr}$  [Eq. (16)] further demonstrates the validity of these arguments and

of the condition  $\varepsilon n^2 \ll 1$  for the reliability of the singular perturbation method.

## References

<sup>1</sup>Flax, A., "Comment on 'Vibration and Buckling of Flexible Rotating Beams'," AIAA Journal, Vol. 34, No. 3, 1996, pp. 640, 641.

Beams'," AIAA Journal, Vol. 34, No. 3, 1996, pp. 640, 641.

<sup>2</sup>Eick, C. D., and Mignolet, M. P., "Vibration and Buckling of Flexible Rotating Beams," AIAA Journal, Vol. 33, No. 3, 1995, pp. 528–538.

<sup>3</sup>Abramowitz, M., and Stegun, I. A., *Handbook of Mathematical Functions*, 9th ed., Dover, New York, 1972.

## Errata

## Flow Visualization Using Natural Condensation of Water Vapor

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[AIAA Journal, 33(11), pp. 2234–2236 (1995)]

HE figures were illegible. They are reproduced below.

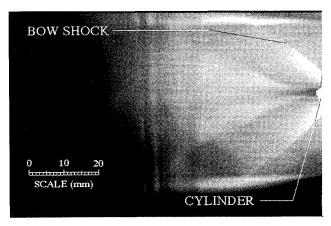


Fig. 1 Flow over a circular cylinder with Mach 2.0 nozzle.

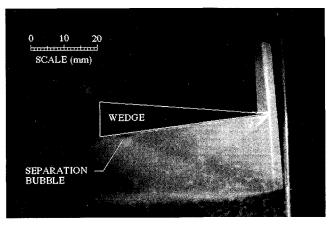


Fig. 2 Flow over a 5.8-deg half-angle wedge with Mach 2.0 nozzle.

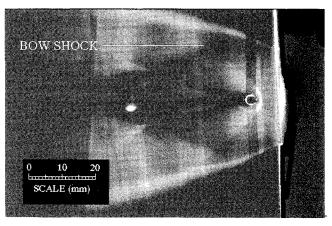


Fig. 3 Flow over a circular cylinder with Mach 1.5 nozzle.

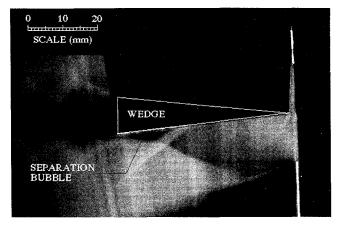


Fig. 4 Flow over a 5.8-deg half-angle wedge with Mach 1.5 nozzle.